THE LANDING AT PMG

EAST RAY ROAD MESA, ARIZONA

PHX17-0119-00
CONCEPTUAL DESIGN
10.09.2017

WARE MALCOMB

architecture | planning | interiors | branding | civil



















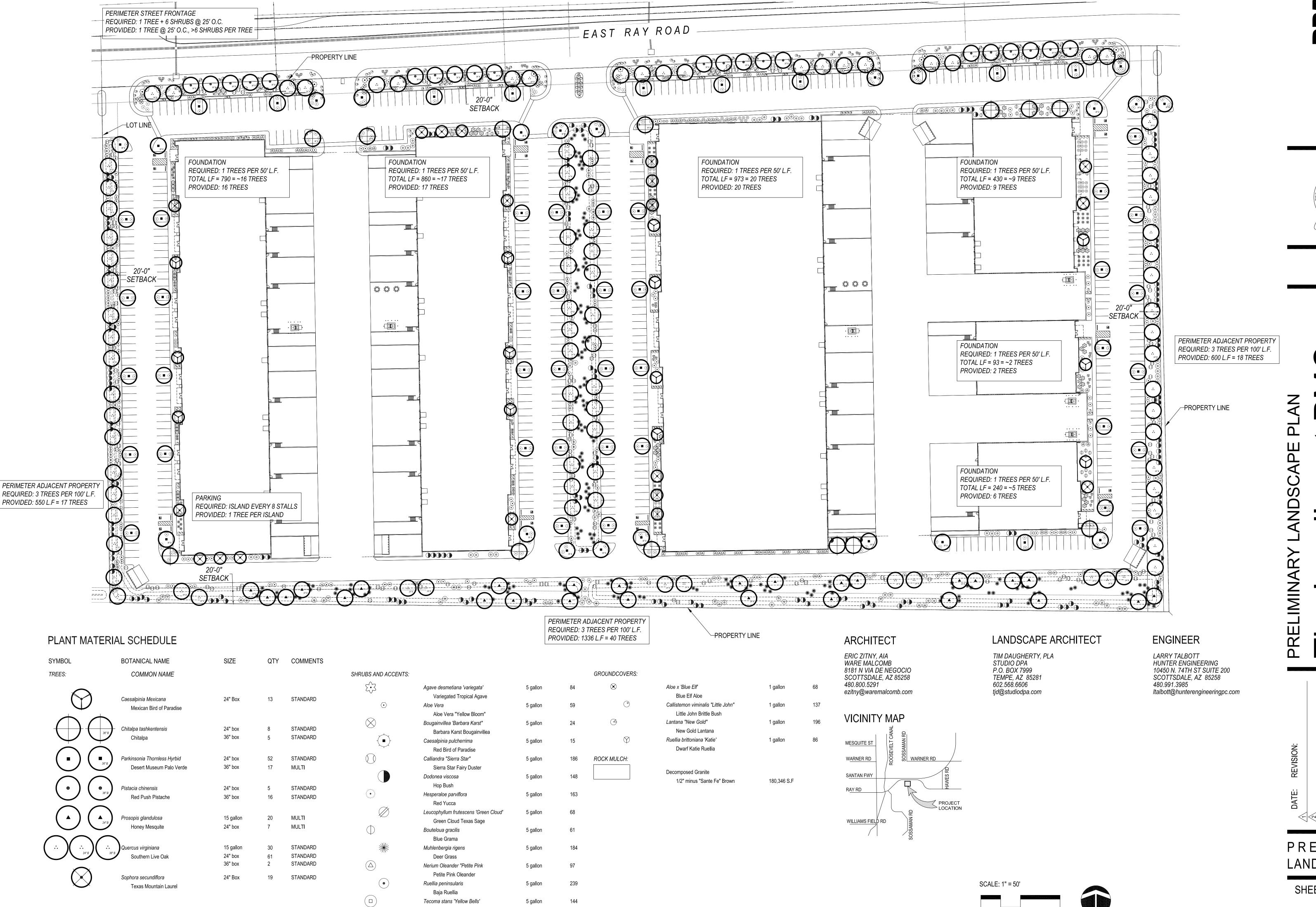




SCHEME 1B

Perspective

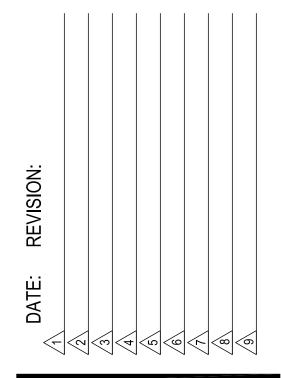




Yellow Bells

DATE:

01.29.18



ME

PRELIMINARY LANDSCAPE PLAN

SHEET 01 OF 01 L1.01

FEMA INFORMATION

THE CURRENT FEMA FLOOD INSURANCE RATE MAP (FIRM) FOR THIS AREA, MAP NUMBER 04013C 2760L (EFFECTIVE REVISED DATE OCTOBER 16, 2013), DESIGNATES THE PROPERTY WITHIN FLOOD HAZARD ZONE X.

ZONE: X IS DEFINED AS AREAS OUTSIDE THE 1% ANNUAL CHANCE FLOODPLAIN, AREAS OF 1% ANNUAL CHANCE SHEET FLOW FLOODING WHERE THE AVERAGE DEPTHS ARE LESS THAN 1 FOOT, AREAS OF 1% ANNUAL CHANCE STREAM FLOODING WHERE THE CONTRIBUTING DRAINAGE AREA IS LESS THAN 1 SQUARE MILE, OR AREAS PROTECTED FROM THE 1% ANNUAL CHANCE FLOOD BY LEVEES. NO BASE FLOOD ELEVATIONS OR DEPTHS ARE SHOWN WITHIN THIS ZONE. INSURANCE PURCHASE IS NOT REQUIRED IN THESE ZONES.

LEGAL DESCRIPTION

THE WEST HALF OF THE SOUTHWEST QUARTER OF SECTION 20, TOWNSHIP 1 SOUTH, RANGE 7 EAST, OF TEN GILA AND SALT RIVER BASE AND MERIDIAN, MARICOPA COUNTY, ARIZONA EXCEPT THAT PORTION OF SAID WEST HALF OF THE SOUTHWEST QUARTER DESCRIBED AS FOLLOWS: BEGINNING AT THE

SOUTHWEST COMER OF SAID SECTION 20; THENCE NORTH O DEGREES 52 MINUTES 41 SECONDS WEST ALONG THE WEST LINE OF SAID SECTION A DISTANCE OF 1415.07 FEET;

THENCE SOUTH 89 DEGREES 38 MINUTES 02 SECONDS EAST A DISTANCE OF 1324.44 FEET;

THENCE SOUTH 0 DEGREES 52 MINUTES 41 SECONDS EAST TO THE SOUTH LINE OF SAID SECTION 20, A DISTANCE OF 1415.07 FEET;

THENCE NORTH 89 DEGREES 38 MINUTES 02 SECONDS WEST ALONG THE SOUTH LINE OF SAID SECTION, A DISTANCE OF 1324.44 FEET TO THE SOUTHWEST COMER, BEING THE TRUE POINT OF BEGINNING;

ALSO EXCEPT THAT PORTION OF THE NORTH HALF OF THE NORTHWEST QUARTER OF THE SOUTHWEST QUARTER OF SECTION 20, TOWNSHIP 1 SOUTH, RANGE 7 EAST, OF THE GILA AND SALT RIVER BASE AND MERIDIAN, MARICOPA COUNTY, ARIZONA, WHICH LIES NORTH OF THE FOLLOWING DESCRIBED LINE:

LINE DESCRIPTION

COMMENCING AT A 1 INCH REBAR MARKING THE WEST QUARTER COMER OF SAID SECTION 20 FROM WHICH A WILLIAMS AIR FORCE BASE (W.A.F.B.) BRASS CAP MARKING THE SOUTHWEST COMER OF SAID SECTION 20 BEARS SOUTH 0

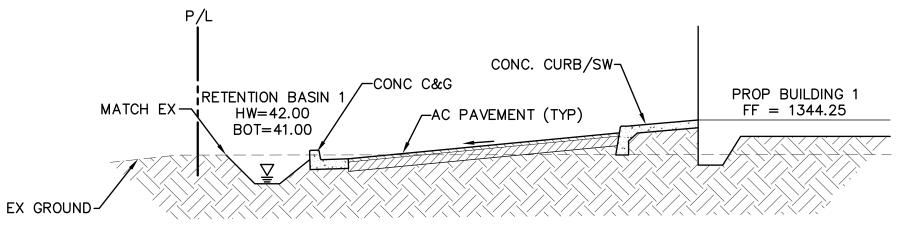
DEGREES 56 MINUTES 06 SECONDS EAST 2629.52 FEET; THENCE ALONG THE WEST LINE OF SAID SECTION 20 SOUTH 0 DEGREES 56 MINUTES 06 SECONDS EAST 424.27 FEET TO

THE POINT OF BEGINNING; THENCE NORTH 87 DEGREES 51 MINUTES 49 SECONDS EAST 979.05 FEET;

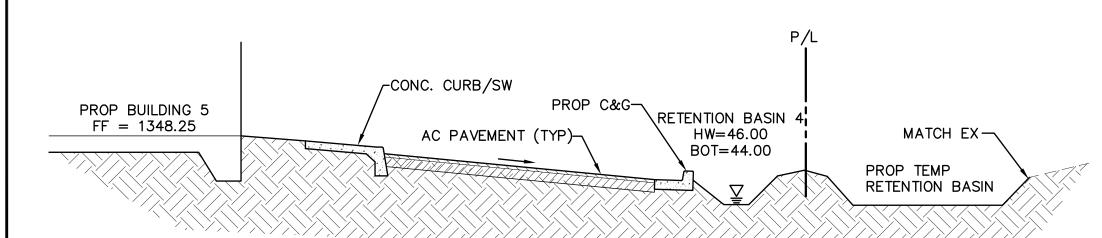
THENCE FROM A LOCAL TANGENT BEARING OF NORTH 89 DEGREES 52 MINUTES 51 SECONDS EAST ALONG A CURVE TO THE LEFT, HAVING A RADIUS OF7879.44 FEET, A LENGTH OF 1699.77 FEET TO THE POINT OF ENDING ON THE NORTH-SOUTH MID-SECTION LINE OF SAID SECTION 20 FROM WHICH A GENERAL LAND OFFICE (G.L.O.) BRASS CAP MARKING THE SOUTH QUARTER CORNER OF SAID SECTION 20 BEARS SOUTH 0 DEGREES 27 MINUTES 46 SÉCONDS EAST 2450.09 FEET.

ABBREVIATIONS

APN	ASSESSOR PARCEL NUMBER	Р	PAVEMENT
B/C	BACK OF CURB	PAE	PUBLIC ACCESS EASEMENT
BÓT	BOTTOM	PDE	PUBLIC DRAINAGE EASEMENT
BRW	BOTTOM OF RETAINING WALL	P	PROPERTY LINE
BVC	BEGINNING OF VERTICAL CURVE	POB	POINT OF BEGINNING
	CONCRETE	POC	POINT OF COMMENCEMENT
C Q	CENTERLINE	PUE	PUBLIC UTILITY EASEMENT
ČF	CUBIC FEET	PUFE	PUBLIC UTILITY FACILITIES EASEMENT
C&G	CURB & GUTTER	PVI	POINT OF VERTICAL INTERSECTION
CY	CUBIC YARD	PVMT	PAVEMENT
DE	DRAINAGE EASEMENT	P\C	PAVEMENT/CONCRETE
DW	DRYWELL	RCW	RECLAIMED WATER
EA	EACH	R/W	RIGHT OF WAY
EL	ELEVATION		
EP	EDGE OF PAVEMENT	SD	STORM DRAIN
ESMT		SF	SQUARE FEET
	EASEMENT CLUBY	SS	SANITARY SEWER
EVC	END OF VERTICAL CURVE	S/W	SIDEWALK
EX	EXISTING	STA	STATION
EXG	EXISTING GRADE	SY	SQUARE YARDS
F/C	FACE OF CURB	TC	TOP OF CURB
FF	FINISH FLOOR	TEL	TELEPHONE
FG	FINISH GRADE	TF	TOP OF FOOTING
FL	FLOWLINE	THR	TOP OF HANDRAIL
FT/FT	FOOT PER FOOT	TPOB	TRUE POINT OF BEGINNING
FM	FORCE MAIN	TRW	TOP OF RETAINING WALL
G	GUTTER	TS	TRAFFIC SIGNAL
GB	GRADE BREAK	TW	TOP OF WALL
GR	GRATE	UGFO	UNDERGROUND FIBER OPTIC
HP	HIGH POINT	UGE	UNDERGROUND ELECTRIC
HW	HIGH WATER	UGT	UNDERGROUND TELEPHONE
IE	INVERT ELEVATION	UTS	UNDERGROUND TRAFFIC SIGNAL
İRR	IRRIGATION	VCP	VITRIFIED CLAY PIPE
LF	LINEAR FEET	VG	VALLEY GUTTER
LIE	LANDSCAPE IRRIGATION EASEMENT	VNAE	VEHICULAR NON-ACCESS EASEMENT
LP	LOW POINT	VOL	VOLUME
MCR	MARICOPA COUNTY RECORDER	VP	VOLUME PROVIDED
ML		VR VR	
M. M_	MATCH LINE		VOLUME REQUIRED
	MONUMENT LINE	W	WATER
MUTE	MULTI USE TRAIL EASEMENT	WLE	WATER LINE EASEMENT
NTS	NOT TO SCALE	WTP	WATER TREATMENT PLANT
OHE	OVERHEAD ELECTRIC	WWTP	WASTEWATER TREATMENT PLANT



TYPICAL SECTION



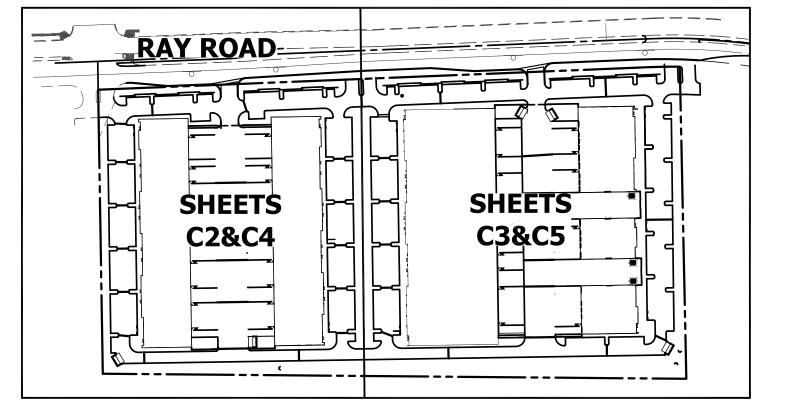
TYPICAL SECTION

CONCEPTUAL GRADING, DRAINAGE AND UTILITY PLAN

THE LANDING AT PMG PHASE I

AT THE SEC OF RAY RD & SOSSAMAN ROAD, MESA, ARIZONA

THE WEST HALF OF THE SOUTHWEST QUARTER OF SECTION 20, TOWNSHIP 1 SOUTH, RANGE 7 EAST, OF THE GILA AND SALT RIVER BASE AND MERIDIAN, MARICOPA COUNTY, ARIZONA



MAP INDEX

SHEET INDEX	CIVIL SHEET
COVER SHEET	C1
CONCEPTUAL GRADING & DRAINAGE PLANS	C2-C3
CONCEPTUAL UTILITY PLANS	C4-C5

PROPOSED LEGEND EXISTING LEGEND

RIGHT OF WAY		DIRECTION OF SLOPE	←
PROPERTY LINE		SEWER LINE	
CENTERLINE		WATER LINE	
EASEMENT LINE		FIRE LINE	
WATER LINE	8" ACP W	EASEMENT	
WATER LINE	16" ACP W	SAWCUT	
SANITARY SEWER LINE	6" VCP SS	GRADE BREAK	\rightarrow
SPOT ELEVATION	+ 1349.16 P	CATCH BASIN	
FIRE HYDRANT		DRYWELL	
WATER VALVE	\otimes	SPOT ELEVATION	90.50P
IRRIGATION CONTROL VALVE	ICV ⊗		<u> </u>
SANITARY SEWER MANHOLE	S	SECTION CALLOUT	(C3)
SANITARY SEWER CLEANOUT	\varnothing	FLOW LINE	→ · · −
SIGN	- o-	BACKFLOW PREVENTOR	\bowtie
LIGHT POLE	$\sim - \sim$	TAPPING SLEEVE & VALVE	 ⊗
ELECTRICAL RISER	E	SANITARY SEWER CLEANOUT	0
ELECTRICAL CABINET	CAB		

OWNER

MARWEST ENTERPRISES, LLC 6710 N. SCOTTSDALE RD 140 SCOTTSDALE, ARIZONA 85253 CONTACT: DAVID MARTENS, JD/MBA PHONE: (602) 390-5403

ARCHITECT

WARE MALCOMB 8181 N VIA DE NEGOCIO SCOTTSDALE, ARIZONA 85258 PHONE: (480) 800-5291 PHONE: (480) 767-1001 CONTACT: ERIC ZITNY, AIA EMAIL: EZITNY@WAREMALCOMB.COM

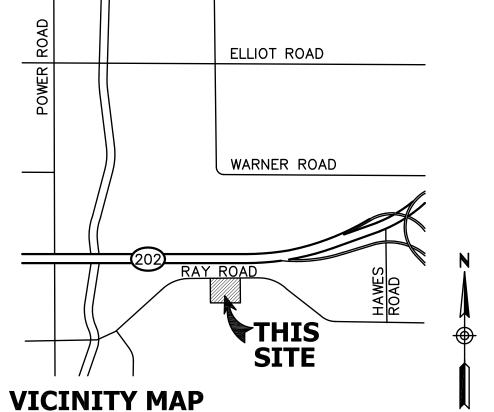
CIVIL ENGINEER

HUNTER ENGINEERING, INC. 10450 N. 74TH STREET, SUITE #200 SCOTTSDALE, ARIZONA 85258 PHONE: (480) 991-3985 CONTACT: JEFF NORMAN, P.E. EMAIL: JNORMAN@HUNTERENGINEERINGPC.COM

RETENTION CALCULATIONS

	AREAS	
ON-SITE AREA		20.89 AC
	ON-SITE	
REQUIRED		
· (0)*(D)*(1)		
$V_{R}=(C)*(\frac{D}{12})*(1)$		

$V_R = (0.90)x(\frac{2.2}{12})x(20.89)x(43,560)$	150,145 CF
PROVIDED	
BASIN 1	16,059 CF
BASIN 2	12,260 CF
BASIN 3	64,135 CF
BASIN 4	12,941 CF
BASIN 5	40,256 CF
96"ø UG RETENTION - 90 LF	4,523 CF
TOTAL	150,174 CF
EXCESS RETENTION	29 CF



SITE ACREAGE

GROSS AREA = 22.93 ACRES NET AREA = 20.89 ACRES

APN#

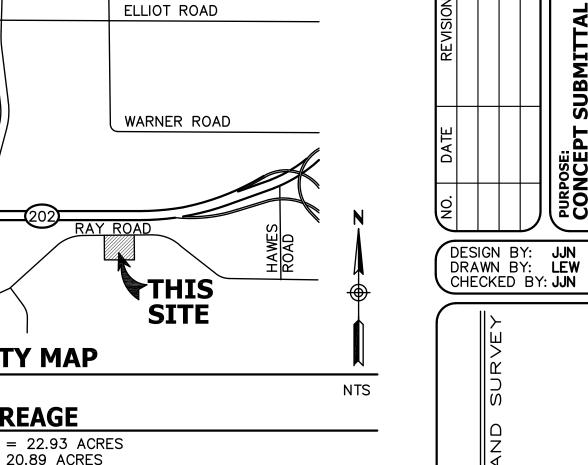
304-30-020J

BENCHMARK

BRASS TAG ON THE TOP OF CURB AT THE NORTHEAST CORNER OF POWER ROAD & HIGHWAY 202 FREEWAY WITH AN ELEVATION OF 1324.10 (NAVD88 DATUM).

BASIS OF BEARING

N87°39'17" E AS MEASURED ALONG THE CENTERLINE OF RAY ROAD RECORDED IN BOOK 1101, PAGE 49, OF OFFICIAL RECORDS, MARICOPA COUNTY, ARIZONA



PRELIMINARY PLANS NOT FOR CONSTRUCTION



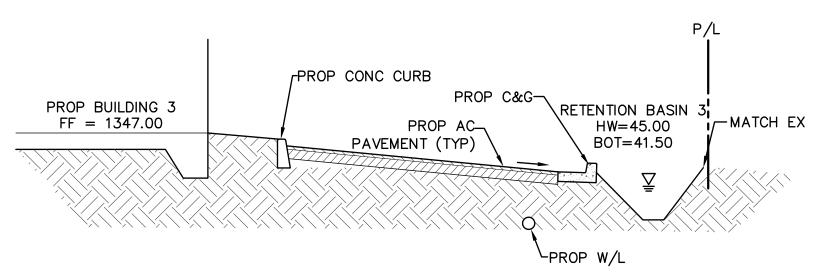
AR ZONA811

BLUE STAKE, INC.

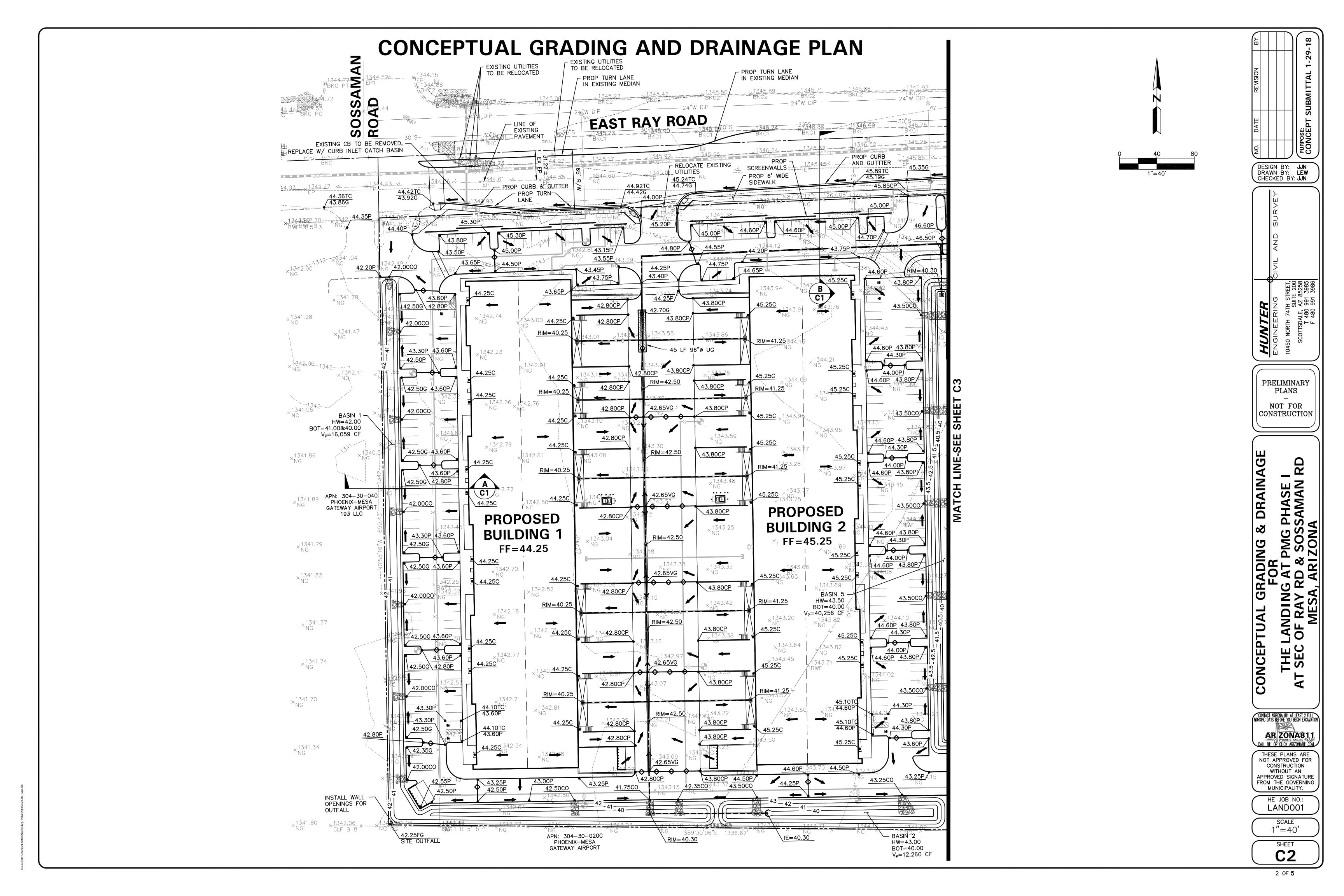
NOT APPROVED FOR CONSTRUCTION WITHOUT AN APPROVED SIGNATURE FROM THE GOVERNING MUNICIPALITY.

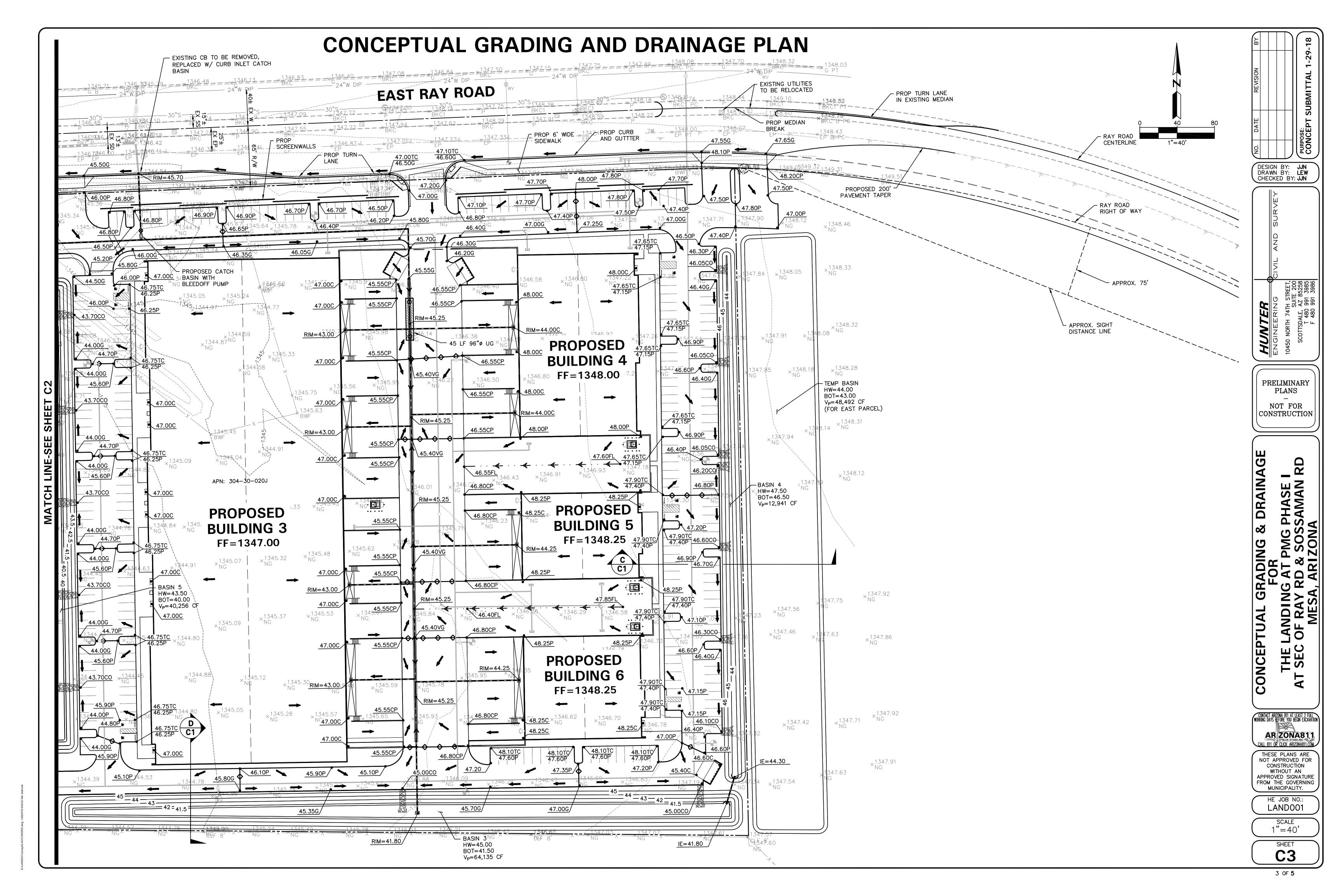
HE JOB NO.: LAND001

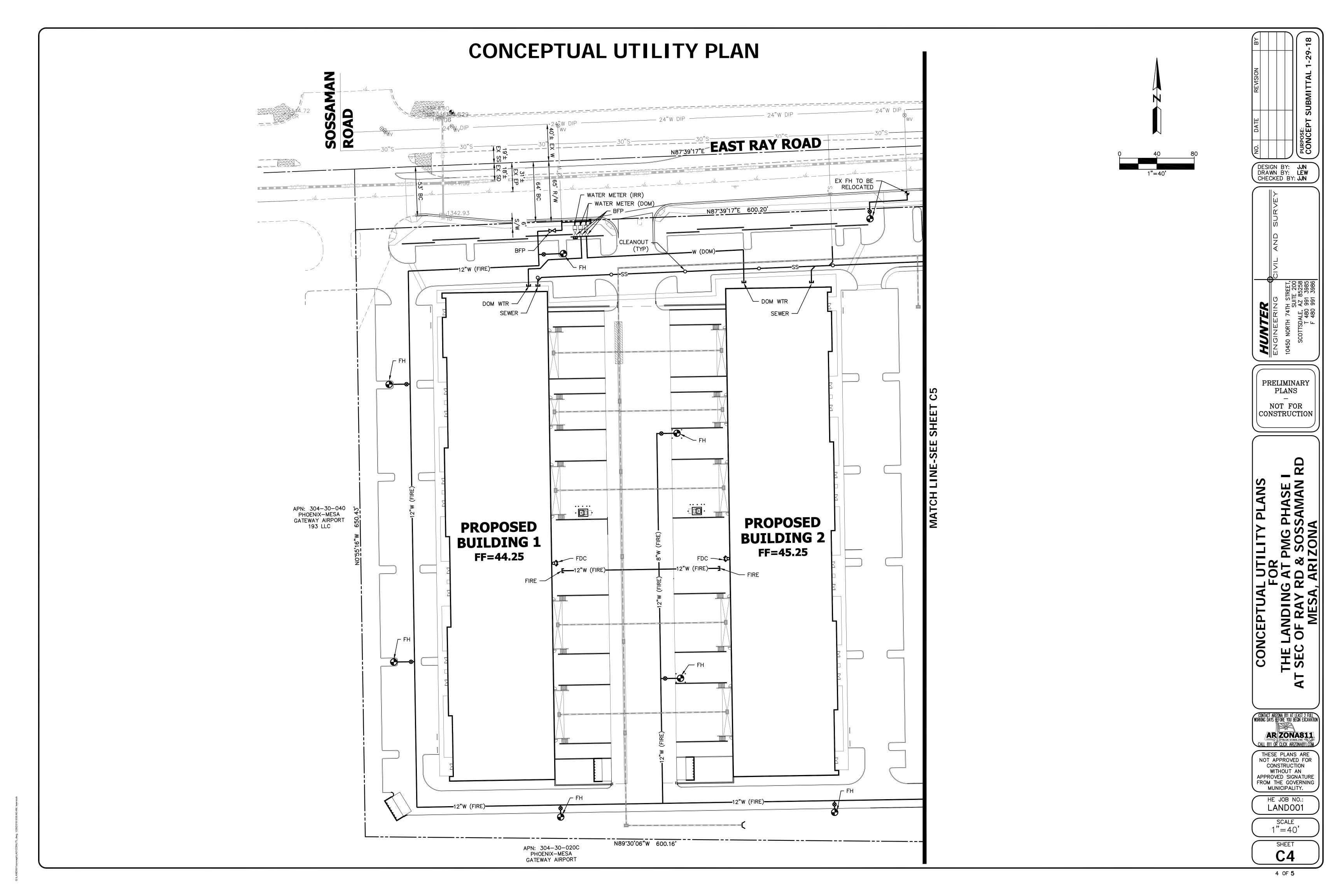
RAY ROAD 65' R/W -EX MEDIAN PROP CONC CURB/SW PROP C&G T PROP 6' S/WT PROP AC PAVEMENT (TYP) PROP BUILDING 2 FF = 1345.25EX AC PVM TYPICAL SECTION

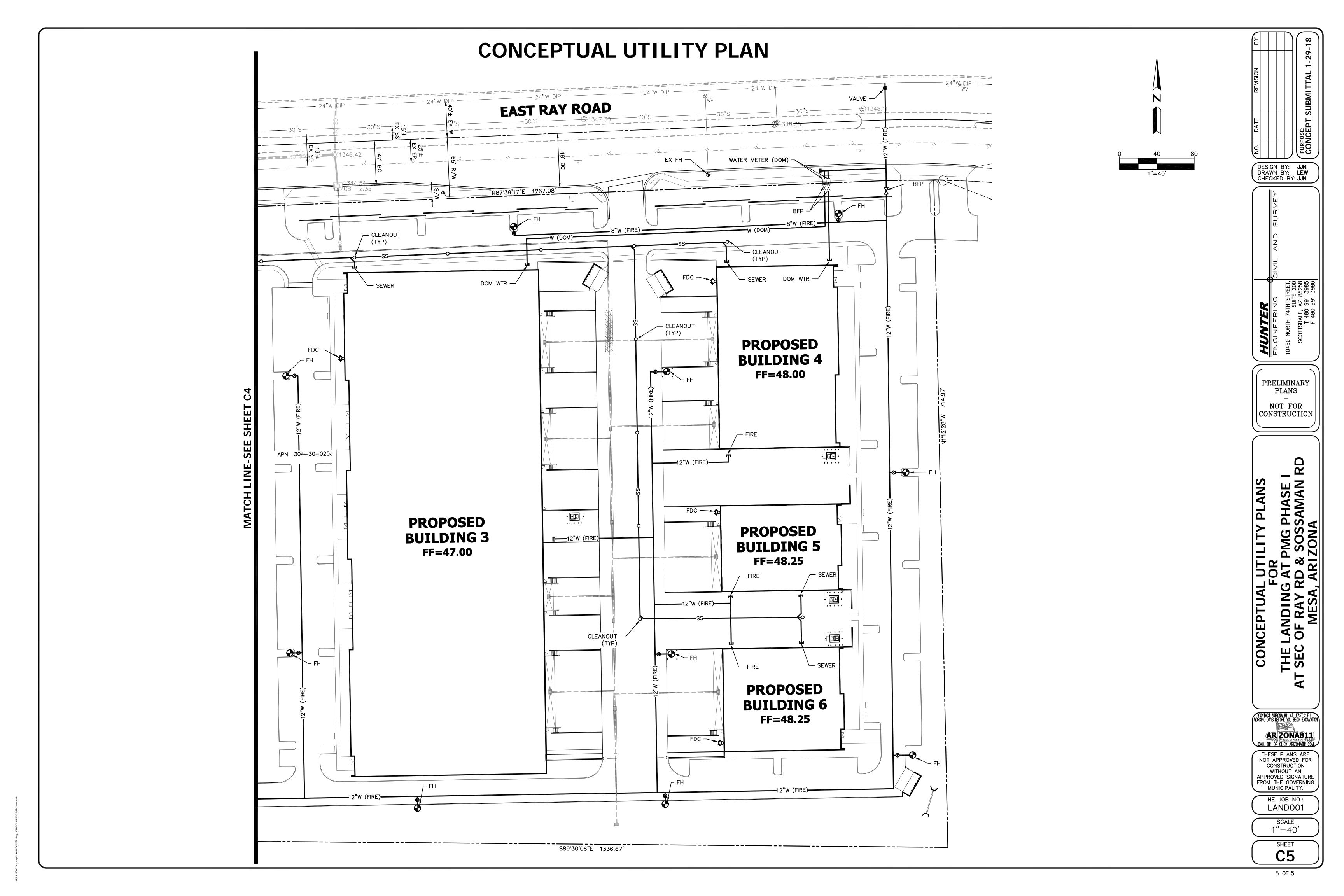


TYPICAL SECTION



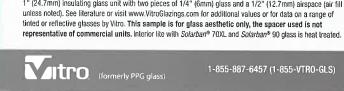












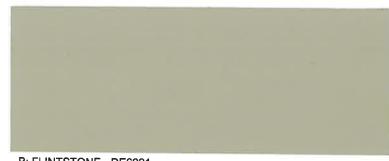
VITRO AZURIA GLAZING



STANDARD PAINTED C: EXPRESSO MACCHIATO - DET680



A: CRYSTAL HAZE - DE6219



B: FLINTSTONE - DE6221



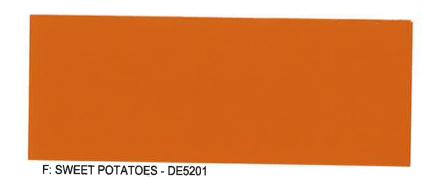
C: EXPRESSO MACCHIATO - DET680



D: COAL MINER - DET613



E: BLACK POOL - DE6315



MATERIALS BOARD





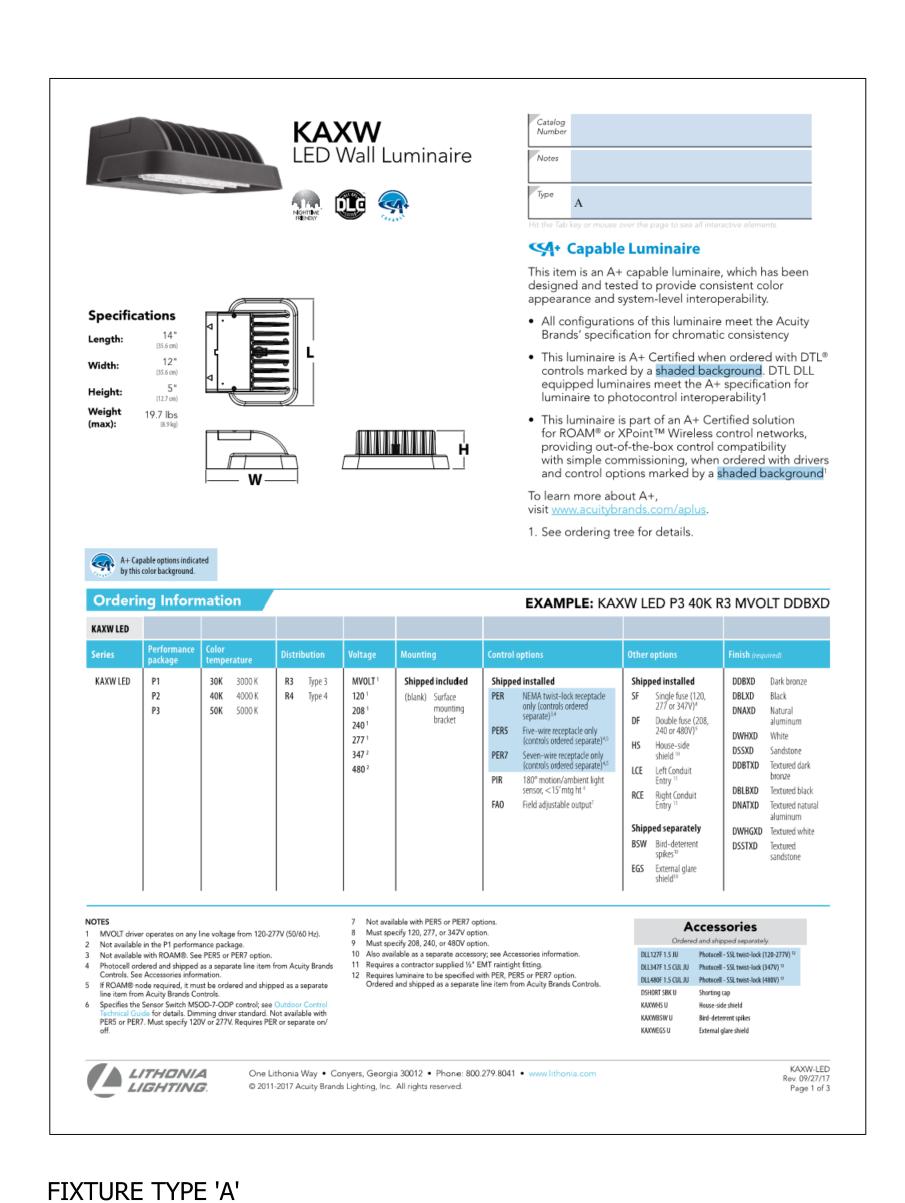
Date: 12.20.2017 To: City of Mesa

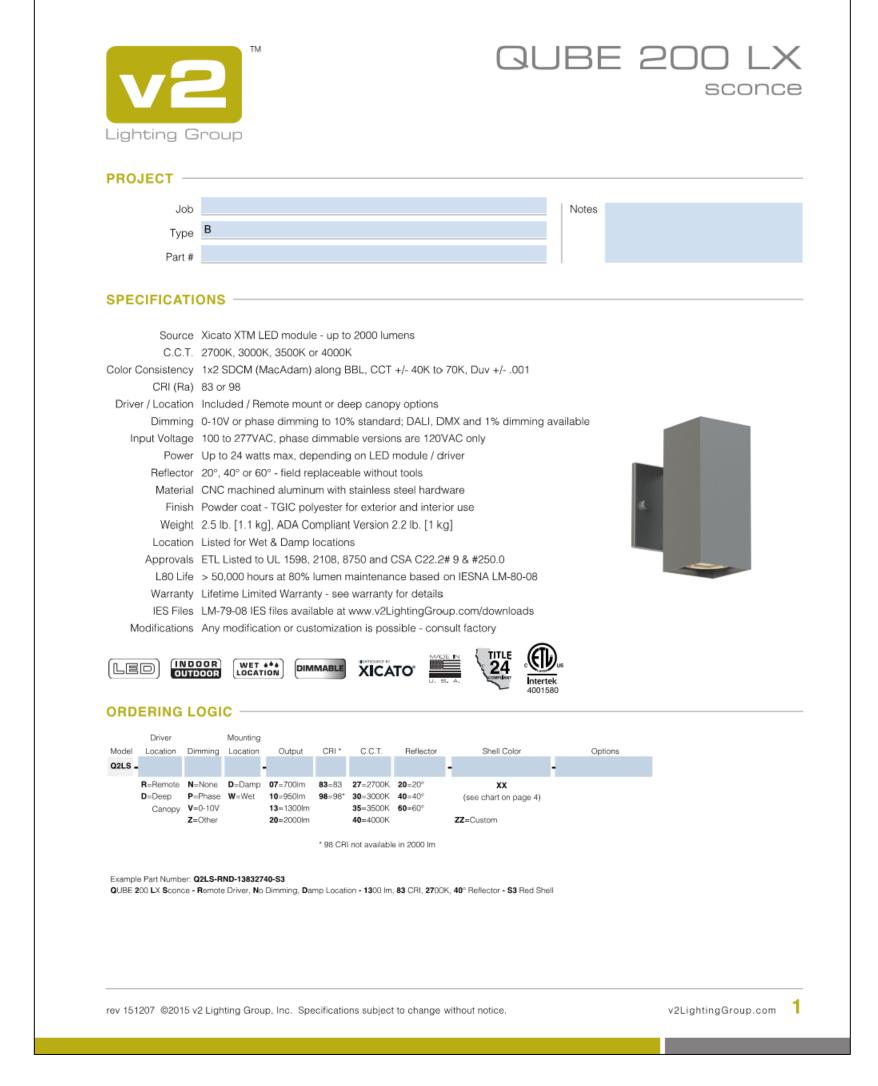
Project Name: The Landing Project No.: PHX17-0119-00 Subject: Project Narrative

From: Eric Zitny

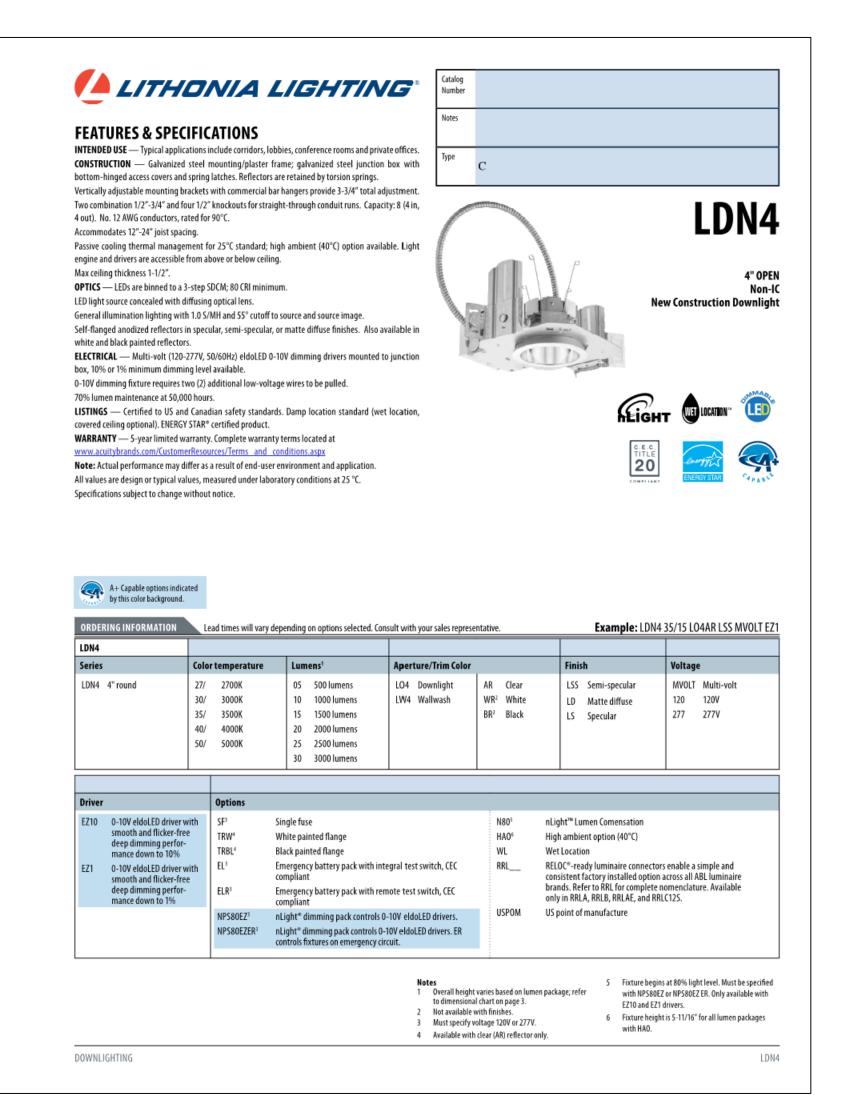
Project Narrative:

The Landing at PMG is a Class A Industrial Park located adjacent to the Phoenix-Mesa Gateway Airport in Mesa, Arizona. The Landing benefits from South Loop 202 visibility as well as direct access along Ray Road. The goal of Phase I of the project is to deliver 275,000 square feet of highly functional and affordable industrial, manufacturing and distribution space to the Southeast Valley. Focusing on the demands of tenants 5,000 to 100,000 square feet, The Landing, with a welcoming and attractive aesthetic, is poised to deliver in 2018 the new standard for industrial space.





FIXTURE TYPE 'C'





FIXTURE TYPE 'SA'

FIXTURE TYPE 'B'

PRELIMINARY NOT FOR CONSTRUCTION OF PLANTS







scheme: 7

The Landing Phase 1 I Photometric Cut Sheets

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1" =40'

0 20 40

(2) LED LUMINAIRES AT 39'-0" MOUNTING E RAY ROAD HEIGHT W/DOUBLE 15' MAST ARMS (TYP)

 $0.4\,0.7\,1.3\,2.2\,2.8\,2.4\,1.6\,0.8\,0.5\,0.4\,0.3\,0.2\,0.3\,0.4\,0.6\,1.0\,2.0\,3.4\,4.1\,3.3\,2.0\,1.2\,0.8\,0.6\,0.4\,0.3\,0.4\,0.6\,0.9\,1.3\,2.3\,3.9\,5.4\,5.1\,3.6\,2.1\,1.4\,1.0\,0.6\,0.5\,0.5\,0.7\,1.1\,1.5\,2.2\,3.6\,5.4\,5.4\,4.8\,2.9\,1.9\,1.4\,1.0\,0.6\,0.5\,0.6\,0.5\,0.6\,1.0\,1.5\,2.0\,2.7\,4.1\,4.7\,4.5\,3.3\,2.3\,1.8\,1.3\,0.8\,0.4\,0.2\,0.1$ 1.6 1.0 0.6 0.4 0.3 0.2 0.2 0.3 0.4 0.5 0.9 1.8 3.0 3.6 2.9 1.7 0.9 0.7 0.5 0.3 0.2 0.2 0.3 0.6 0.8 1.3 2.2 3.9 5.1 4.4 2.7 1.6 1.0 0.7 0.4 0.5 0.2 0.2 0.5 0.6 0.9 1.3 1.8 2.3 3.1 4.0 4.3 3.7 2.8 2.2 1.7 1.2 0.8 0.6 0.8 1.2 1.7 2.3 2.8 3.2 3.6 3.4 3.0 2.6 2.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.2 0.1 1.8 1.2 0.7 0.6 0.9 1.3 1.8 2.3 3.1 4.0 4.3 3.7 2.8 2.2 1.7 1.2 0.8 0.6 0.8 1.2 1.7 2.3 2.8 3.2 3.6 3.4 3.0 2.6 2.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.2 0.1 1.8 1.2 0.7 0.6 0.9 1.3 1.8 2.3 3.1 4.0 4.3 3.7 2.8 2.2 1.7 1.2 0.8 0.6 0.8 1.2 1.7 2.3 2.8 3.2 3.6 3.4 3.0 2.6 2.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.9 1.3 1.8 2.3 3.1 4.0 4.3 3.7 2.8 2.2 1.7 1.2 0.8 0.6 0.8 1.2 1.7 2.3 2.8 3.2 3.6 3.4 3.0 2.6 2.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0.5 0.9 1.3 1.8 2.3 3.1 4.0 4.3 3.7 2.8 2.2 1.7 1.2 0.8 0.6 0.8 1.2 1.7 2.3 2.8 3.2 3.6 3.4 3.0 2.6 2.1 1.5 1.0 0.5 0.2 0.1 1.5 1.0 0. $0.1\ \ 0.1\ \ 0.1\ \ 0.1\ \ 0.1\ \ 0.1\ \ 0.2\ \ 0.4\ \ 0.7\ \ 1.3\ \ 2.2\ \ 3.0\ \ 2.8\ \ 1.8\ \ 1.0\ \ 0.7\ \ 0.5\ \ 0.4\ \ 0.5\ \$ 0.1 0.2 0.5 0.8 1.2 $\frac{2.2}{3.9}$ $\frac{5.2}{3.8}$ $\frac{1.2}{3.9}$ $\frac{1.3}{3.1.9}$ $\frac{1.3}{3.1.9}$ $\frac{1.3}{3.1.9}$ $\frac{1.6}{3.1.9}$ $\frac{1.6}{3.1.9}$ $\frac{1.6}{3.1.9}$ $\frac{1.6}{3.1.9}$ $\frac{1.7}{3.1.9}$ $\frac{1.8}{3.1.9}$ $\frac{1.7}{3.1.9}$ $\frac{1.7}{3.1.9}$ $\frac{1.8}{3.1.9}$ $\frac{1.7}{3.1.9}$ $\frac{1.8}{3.1.9}$ $\frac{1.7}{3.1.9}$ $\frac{1.8}{3.1.9}$ $\frac{1.7}{3.1.9}$ $\frac{1.7}{3.1.9}$

 $0.2 \ 0.5$ 1.4 1.8 1.9 1.7 1.3 1.0 0.7 0.6 0.6 0.6 0.6 0.7 0.9 1.1 1.5 1.8 2.0 1.9

BLDG 2

58,688 SF

CLR. HGT: 30'

1.5 1.7 1.8 1.7 2.0 2.6 2.6 3.6 3.9 2.7 1.4 1.1 1.1 1.1 1.2 1.3 1.5 1.5 1. (\0.6 \0.9 \1.\) 1.3 1.4 1.4 1.4 1.4 1.9 2.2 2.1 2.0 2.1 2.4 2.3 3.5 4.1 3.0 1.3 1.0 0.8 0.9 1.2 1.7 1.9 2.2 2.0 0.5 0.8 1.0 1.0 1.1 1. 1.1 1.0 0.5 0.7 1.0 1.1 1.2 1.1 1.1 0.9 2.7 2.8 2.3 2.4 2.4 2.5 2.2 2.9 3.1 1.9 1.0 0.8 0.7 0.8 1.3 2.0 2.0 2.8 2.8 0.6 0.9 1.2 1.4 1.5 1.4 1.2 1.0 L3.73.52.22.201.8 1.9 2.1 2.0 1.0 0.6 0.5 0.6 0.7 1.1 1.8 1.9 3 2 3 4 A 0.71.2 1.5 1.8 1.9 1.7 1.3 1.0 3.6 3.4 2.2 2.0 1.7 1.2 1.2 1.1 0.9 0.5 0.4 0.4 0.5 0.6 1.1 1.8 1.9 3.1 3. 1.0 1.7 2.0 2.2 2.3 1.9 1.4 1.0 . 2.4 2.6 2.2 2.1 1.5 /1.0 0.7 0.6 0.4 0.3 0.3 0.3 0.4 0.6 1.2 1.8 2.1 2.5 2.**3** 1,7,2.92.72.82.72.11.510 1.7 2.0 2.0 1.7 1.2 0.8 0.5 0.4 0.3 0.2 0.2 0.2 0.3 0.6 0.9 1.4 1.8 1.9 1. 1.5 1.9 2.0 1.6 1.1, 0.7 0.4 0.3 0.2 0.1 0.2 0.2 0.3 0.5 0.9 1.4 1.8 1.9 1.6 3.1 5.1 4.2 3.3 3.0 2.3 1.5 0.9 4.3 **4.**万.0 3.8 3.1 2.3 1.5 0.9 2.1 2.4 2.2 2.0 1.4 0.8 0.4 0.2 0.2 0.1 0.1 0.2 0.3 0,5 1.1 1.8 2.1 2.4 2.3 4.0 6.0 4.9 3.7 3.1 2.3 1.5 0.9 3.2 3.2 2.2 1.9 1.4 0.7 0.3 0.2 0.1 0.1 0.2 0.2 0.5 1.0 1.8 1.9 3.0 3.3

2.6 4.3 3.5 3.1 2.9 2.2 1.5 0.9 \[\frac{3}{.6}\frac{3.4}{2.2}\frac{1.8}{1.8}\frac{1.4}{0.7}\frac{0.3}{0.3}\frac{0.2}{0.1}\frac{0.1}{0.1}\frac{0.1}{0.1}\frac{0.1}{0.2}\frac{0.5}{1.0}\frac{1.8}{1.8}\frac{3.1}{3.1}\frac{3}{0.6}\frac{6}{3.6}\frac{3.4}{0.7}\frac{0.5}{0.1}\frac{0.1}{ 1.4 2.3 2.3 2.6 2.5 2.0 1.4 0.9 2.72.82.22.01.50.80.30.20.10.10.10.10.10.20.51.11.92.02.72.8 | 1.7 2.1 2.1 1.7 1.2 0.7 0.3 0.2 0.1 0.1 0.1 0.1 0.2 0.5 0.9 1.5 1.9 2.2 1.9 0,814 1.7 2.0 2.1 1.8 1.3 0.9 0.6101.21.51.61.41.108 1.3 1.7 1.9 1.5 1.0 0.6 0.3 0.2 0.1 0.1 0.1 0.1 0.2 0.5 0.8 1.3 1.7 1.<u>8 1.5</u> 0.3 0.6 0.8 0.9 1.0 1.0 0.8 0.7 0.1 0.3 0.4 0.5 0.6 0.6 0.5 0.5 2.7 2.9 2.3 1.9 1.5 0.8 0.3 0.2 0.1 0.1 0.1 0.1 0.2 0.4 1.0 1.8 1.9 2.7 2.9 0.1 0 1 0.2 0.2 0.3 0.3 0.3 0.3 **A** 6 3.4 2.3 1.8 1.4 0.7 0.3 0.2 0.1 0.1 0.1 0.1 0.2 0.4 0.9 1.7 1.8 3.0 3.6 A 0.0 0.0 0.1 0.1 0.1 0.1 0.1 0.2 3.1 3.2 2.4 1.9 1.5 0.7 0.3 0.2 0.1 0.1 0.1 0.1 0.2 0.4 1.0 1.8 1.9 2.9 3.2

0.0 0.0 0.0 0.0 0.0 0.1 0.1 0.1 1.9 2.3 2.2 1.9 1.4 0.8 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.5 1.0 1.6 2.0 2.4 2.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.3 1.7 1.9 1.6 1.0 0.7 0.3 0.2 0.1 0.1 0.1 0.1 0.2 0.4 0.8 1.2 1.7 1.9 1.6 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 1.3 1.8 2.0 1.6 1.1 0.7 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.4 0.8 1.3 1.7 2.0 1.8 0.0 0.0 0.0 0.0 0.0 0.0 0.0 2.0 2.5 2.3 2.0 1.6 0.9 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.4 1.0 1.7 2.0 2.4 2.5 BLDG 1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 6 3.1 3.3 2.5 1.8 1.5 0.8 0.3 0.2 0.1 0.1 0.1 0.1 0.2 0.4 0.9 1.7 1.8 2.8 3.4 3.3 3.4 2.5 1.8 1.5 0.8 0.3 0.2 0.1 0.1 0.1 0.1 0.2 0.4 0.9 1.7 1.8 2.8 3.5 58,688 SF d q. d o. d o. d o. d o. d o, d o, d

CLR. HGT: 30'

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0.41.01.51.72.02.01.71.30.9

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2.6 2.5 2.0 1.8 1.0 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.3 0.9 1.6 2.0 2.3 2.7 2.3 3.5 2.8 1.8 1.7 0.9 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.3 0.7 1.5 1.8 2.4 3.4 3.4 2.8 1.8 1.7 0.9 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.3 0.8 1.5 1.8 2.5 3.3 3.2 2.4 2.4 2.0 1.7 1.0 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.4 0.8 1.5 2.0 2.3 2.4 2.0 118 2.0 1.7 1.3 0.8 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.4 0.7 1.1 1.6 1.9 1.8 1.3 2.2 2.4 2.0 1.7 1.0 0.5 0.2 0.1 0.1 0.1 0.1 0.2 0.3 0.8 1.4 2.0 2.2 2.4 2.0 3.2 2.9 1.9 1.7 1.0 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.3 0.7 1.4 1.9 <u>2.3 3.2</u> 3.2 3.0 1.8 1.7 1.0 0.4 0.2 0.1 0.1 0.1 0.2 0.3 0.7 1.4 1.8 2.3 3.4 3.6 2.9 2.7 1.9 1.8 1.1 0.5 0.2 0.1 0.1 0.1 0.1 0.2 0.3 0.8 1.6 2.0 2.3 2.9 2.6 __2.0 <u>2.2</u> 1.9 1.5 0.9 0.5 0.3 0.2 0.1 0.1 0.1 0.2 0.4 0.7 1.2 1.7 <u>2.</u>1 2.1 1,64 1.9 2.1 1.9 1.5 1.0 0 6 0.4 0.3 0.2 0.2 0.2 0.3 0 4 0.7 1.2 1.8 2.1 2.1 1 8 <u>__2.7</u> 2.7 2.1 2.1 1.3 0 7 0.4 0.3 0.3 0.3 0.3 0.4 0 5 0.9 1.6 2.1 2.2 2.9 2 7

Δ 3.6 3.3 2.0 2.0 1.4 0.8 0.6 0.5 0.5 0.5 0.5 0.6 0.7 1.0 1.7 2.1 2.3 3.5 3 λ

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2.3 2.5 2.2 2.3 1.8 1.4 1.3 1.2 1.2 1.2 1.2 1.3 1.4 1.6 2.0 2.3 2.3 2.4 2 1

1.3 1.6 1.7 1.8 1.7 1.8 1.8 1.9 1.9 1.9 1.9 1.9 1.8 1.9 1.8 1.9 1.7 1.5 1.2

+C 1.2 1.5 1.8 2.1 2.0 1.9 1.7 1.4 1.1 1.2 1 5 1.7 1.9 2.0 1.9 1.6 1 2 1.0 1.9 2.3 2.4 2.2 2.1 1.7 1.3 1.4 1.9 2.1 2.3 2.4 2.1 1.6 1.2 0.9 1.0 1.4 2.0 2.6 2.8 2.7 2.8 2.4 2.0 2.0 2 7 2.7 2.7 2.8 2.3 1.7 1 2 0.8 0.9 1.3 2.0 2.9 3.2 3.6 4.6 3.9 3.2 3.4 4 5 4.2 3.4 3.1 2.6 1.7 1.1 0.7 0.8 1.3 2.0 2.9 3.5 4.6 6.2 5.7 4.7 4.9 6.0 5.6 4.1 3.3 2.6 1.7 1.1 0.7 0.8 1.3 2.0 2.9 3.5 4.7 6.1 5.9 4.9 5.1 6.2 5.6 4.2 3.3 2.6 1.7 1.1 0.7 <u>, 0.8 1.3</u> 2.0 2.8 3.<u>2 3.9 5.1 4.4 3.6 3.8/5 1 4.6 3.6 3.2 2.5 1.7 1.1</u> 0.7 0.9 1.3 1.9 2.6 2.8 2.8 3.0 2.6 2.1 2.2 3 0 2.9 2.8 2.8 2.3 1.6 1.1 0.7 C | 0.9 1.3 1.7 2.2 2.4 2.1 2 0 1 6 1 1 1.2 1 8 2.0 2.2 2.4 2.1 1.5 1.1 0.7 0.5 (C) 1.0 1.2 1.6 1.9 1.9 1.7 1,5 1.1 0.7 0.8 1.2 1.5 1.8 1.9 1.8 1.5 1.1 0.8 0.5 0.7 0.6 0.6 0.8 1.2 1.4 1.6 1.5 1.3 1.1 0.7 0.6 0.6 0.8 1.2 1.4 1.6 1.6 1.4 1.1 0.9 6. 6 1.01.21.41.51.41.21.00,60.50.50,61.01.31.51.51.41.10.97:0 1.0 1.2 1.6 1.9 1.9 1.7 1.5 1.1 0.7 0.8 1.2 1.5 1.8 2.0 1.9 <u>1.6 1.2</u> 0.9 4.6 1.0 1.2 1.7 2.2 2.<u>4 2.2 2</u>0 1.6 1.2 1.2 1.7 <u>2.1 2</u>.2 2.5 2.2 <u>1.7 1.2</u> 0.8 4.8 C 1 0 1.3 1.8 2.6 2.8 2.8 3 1 2.8 2 2 2.2 2 9 3.2 2.9 2.9 2.5 1.8 1.2 0.8 3

0.8 1.2 1.9 2.8 3.2 3.9 5 2/4.6 3 7 3.8 4.7 5.2 3.9 3.2 2.8 1.9 1.2 0.8 5.8 0.8 1.2 1.9 2.8 3.4 4.6 5 95 5.9 4.7 4.7 6. (5.5.8 4.5 3.4 2.8 1.9 1.2 0.7 5.8 13 1.2 1.9 2.8 3.3 4.3 5.9 **5.5** 4 3 **4.3** 5.4 5.8 4 2 3.3 2.8 1.9 1.2 0.7 5.4 3 8 1.2 1.8 2.7 3.0 3.3 4.1 3.7 2.9 2 8 3.7 3.9 3.3 3.0 2.6 1.8 1.2 0.7 0.6 4.41.21.72.32.62.52.4211.61.62.12.42.52.62.31.71.20.80.5 \$\frac{4}{2}\frac{1}{1}\frac{1}{5}\frac{5}{2}\frac{1}{1}\frac{1}{5}\frac{1}{2}\frac{1}{1}\frac{1}{2}\frac{1}\frac{1}{2}\f (本31.01.31.61.61.41.20.90.6060.91.31.51.71.71.41.20.98.8

080.80.91.01.00.90.8050.4050.61.01.21.41.51.41.21.085 0.5 0.6 0.8 0.9 0.9 0.8 0.6 0.3 0.3 0.4 0.5 0.9 1.2 1.4 1.5 1.4 1.2 1.0 85 060.91.11.41.41.31.10170.4040.71.11.41.61.71.51.31.086 ·C 1.5 1.0 1.4 1.8 2.0 1.8 1.5 1.2 0.6 0.5 1.0 1.5 1.8 2.1 2.0 1.7 1.3 0.9 21 c 1.4 1.1 1.6 2.1 2.5 2.3 2.1 1.8 1.0 0.9 1.6 2.2 2.3 2.5 2.4 1.8 1.3 0.9 0.6 1.2 1.1 1.7 2.5 3.1 3.8 5.2 5.0 3.1 2.6 4 6 5.8 4.3 3.3 2.9 2.0 1.3 0.8 2.50 1.4 1.0 1.7 2.6 3.2 4.2 5.3 5.5 3.6 2.9 5.1 5.7 4.6 3.5 2.9 2.0 1.3 0.8 1.9 7.4 1.0 1.6 2.5 3.1 3.6 4.8 4.8 2.8 2.2 3.9 5.2 3.9 3.2 2.8 1.9 1.3 0.8 1.8 1.0 1.6 2.3 2.8 2.8 3.0 2.9 1.6 1.3/2.3 3.0 2.8 2.8 2.6 1.9 1.3 0.8 1.5 1.0 1.5 2.0 2.4 2.2 1.9 1.6 0.8 0.7 1.3 1.9 2.1 2.4 2.3 1.8 1.3 0.9 1.7

<u>0.91.</u>31.71.91.71.41.10.50.50.91.41.61.91.91.61.20.91.8 D.8 1.0 1.3 1.3 1.2 1.0 D.6 D.4 D.4 D.6 1.0 1.3 1.5 1.6 1.4 1.2 1.0 2.2 0.6 0.7 0.8 0.8 0.7 0.5 0.4 0.3 0.4 0.5 0.8 1.1 1.3 1.5 1.4 1.2 1.0 2.1 0.7 0.9 1.1 1.2 1.1 0.9 0.7 0.5 0.4 0.6 1.0 1.2 1.4 1.6 1.5 1.3 1.0 1.6 0.9 1.2 1.5 1.7 1.6 1.4 1.1 0.8 0.6 0.9 1.3 1.6 1.8 1.9 1.7 1.4 1.0 0.8 °C 1.0 1.4 1.9 2.2 2.1 1.9 1.7 1.2 1.0 1.3 1.8 2.0 2.3 2.3 1.9 1.4 1.0 0.7 ·c 1.0 1.6 2.2 2.7 2.7 2.7 2.8 2.0 1.9 2.2 2.9 2.7 2.8 2.7 2.1 1.4 1.0 0.6 1.0 1.6 2.4 3.1 3.4 4.3 4.9 3.6 3.2 3.9 <u>5.3 4.0</u> 3.3 3.0 2<u>.2 1.4</u> 0.9 0.6 1.0 1.6 2.5 3.2 4.0 5.4 6.2 4.9 4.5 5.4 6.4 5.0 3.7 3.1 2.2 1.4 0.9 0.6 1.0 1.6 2.5 3.2 4.0 5.3 6.2 4.9 4.4 5.2 6.4 4.9 3.7 3.1 2.2 1.4 0.9 0.6 1.0 1.6 2.4 3.1 3.4 4.1 4.8 3.4 2.9 3.6 4.8 3.8 3.2 3.0 2.2 1.4 0.9 b. |C|| | 1.1 | 1.6 | 2.2 | 2.7 | 2.8 | 2.7 | 2.8 | 3.9 | 1.8 | 2.1 | 2.7 | 2.6 | 2.8 | 2.6 | 2.1 | 1.4 | 0.9 | 0.6 C) | 1.1 1.5 2.0 2.4 2.3 2.0 1.8 1.2 1.0 1.4 1.9 2.1 2.3 2.3 1.<u>8 1.4 1</u>.0 0.6 1.7 2.0 1.8 1.6 1.4 1.0 0.8 1.1 1.4 1.7 1.9 1.9 1.6 1.3 0.9 0.8

C) 0.9 1.2 1.5 1.6 1.5 1.3 1.1 0.9 0.8 0.9 1.2 1.4 1.5 1.6 1.4 1.1 0.8 0.9

0.71.01.21.31.31.21.11.01.01.01.21.31.41.41.30.90.70.8

11

BLDG. 3 108,368 SF

CLR.HGT: 30'

BLDG. 4 25,083 SF CLR.HGT: 24

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3.2 3.3 2.5 1.9 1.5 0.8 0.4 0.3 0.3 0.3 0.3 0.3 0.4 0.6 1.0 1.8 1.9 3.0 3.5

\$\frac{1}{3}.5 \frac{1}{3}.5 \frac{1}{2}.5 \frac{1}{1}.8 \frac{1}{1}.5 \frac{1}{0}.8 \quad 0.4 \frac{1}{0}.3 \frac{1}{0}.2 \frac{1}{0}.2 \frac{1}{0}.2 \frac{1}{0}.3 \frac{1}{0}.3 \frac{1}{0}.5 \frac{1}{1}.0 \frac{1}{1}.7 \frac{1}{1}.9 \frac{1}{2}.9 \frac{1}{3}.4 \quad \frac{1}{0}.5 2.52.8 2.4 2.0 1.6 0.9 0.4 0.2 0.2 0.1 0.2 0.2 0.3 0.5 1.0 1.8 2.0 2.5 5

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.5 2.2 2.3 1.9 1.4 0,8 p.4 0.2 0.1 0.1 0.1 0.1 0.2 p.4 0.9 1.6 2.0 2.4 2.3

2.5 3.0 2.5 1.9 1.6 0.9 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.4 0.9 1.7 1.9 2.7 3.2

<mark>አ</mark>ቶ2 3.5 2.7 1.8 1.6 0.8 p.3 0.2 0.1 0.1 0.1 0.1 0.2 p.4 0.8 1.6 1.8 2.am 5 \$.0 ⁷ - 13.1 2.6 1.9 1.6 0.9 p.4 0.2 0.1 0.1 0.1 0.1 0.2 p.4 0.9 1.7 1.9 2.5 2.8 2.

2.2 <u>2.3</u> 1.9 1.5 0.8 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.4 0.8 1.4 <u>1.8 2.2 2.</u>0 **1**,

1.6 1.9 1.6 1.1 0.7 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.4 0,7 1.1 1.6 1.8 1.5 0.9

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2.6 2.4 2.0 1.7 1.0 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.4 0.9 1.6 1.9 2.4 2.8 2.3

3.4 2.8 1.8 1.6 0 9 0.4 0.2 0.1 0.1 0.1 0.2 0.3 0.7 1.5 1.7 2.5 3.4 3A2

3.4 2.8 1.8 1.7 0.9 \$\dagger\$ 4 0.2 0.1 0.1 0.1 0.1 0.1 \$\dagger\$ 0.7 1.4 1.7 2.4 3.1 \$\frac{1}{2}.7\$

- 2.5 2.4 2.0 1.7 1,0 \$.4 0.2 0.1 0.1 0.1 0.1 0.1 \$.3 0.7 1.4 1.8 2.1 2.1 **j**le

1.5 1.8 1.7 1.3 0.8 0.5 0.2 0.1 0.1 0.1 0.1 0.1 0.3 0.7 1.4 1.9 2.2 3.1 🛪 0

1.97221.9 155 0.9 0.5 0.2 0.1 0.1 0.1 0.1 0.1 0.1 0.2 0.6 1.3 1.8 2.2 3.4 3 6

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🖟 3.6 3.1 1.8 1.8 1.0 ዕ 4 0.2 0.1 0.1 0.1 0.1 0.2 ዕ 3 0.7 1.2 1.8 2.1 2.3 18

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7.6 1.9 1.8 1.3 0.8 0 5 0.2 0.1 0.1 0.1 0.1 0.2 0 3 0.7 1.4 2.0 2.1 <u>2.7 2</u>5

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<u>. 1.4 1.7 1.8 1.4 0.9 0.6 0.3 0.2 0.1 0.1 0.1 0.2 0.3 0.6 1.2 1.8 2.1 2.4 2.</u>

1.5 1.8 1.8 1.5 1.0 0.6 0.3 0.2 0.1 0.1 0.1 0.2 0.3 0.6 0.9 1.4 1.8 1.9 1.6

2.2 2.5 2.1 2.0 1.3 0.7 0.3 0.2 0.1 0.1 0.1 0.2 0.3 0.6 0.9 1.5 1.8 2.0 1.

3.4 3.3 2.1 1.9 1.3 0.7 0.4 0.3 0.2 0.2 0.2 0.3 0.4 0.7 1.3 2.0 2.1 2.6 2.4

^A3.6 3.4 2.2 1.9 1.4 0.8 0.5 0.4 0.3 0.3 0.3 0.4 0.5 0 7 1.3 2.0 2.0 3.2 3.5

2.62.7 2.2 2.1 1.6 1.0 0.6 0.5 0.5 0.5 0.5 0.5 0.6 0.9 1.4 2.1 2.1 3.3 3.6

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<u>1.1 0.6 0.3 0.3 0</u> 2 0.2 0.3 0.4 0.5 1.0 1.9 3.0 3.5 2.7 1.5 0.8 0.6 0.4 0.2 0.2 0.2 0.4 0.7 1.1 2.0 3.6 4.8 4.3 2 7 1.5 1.0 0.7 0.3 0.1 0.1 0.0

5.71.1 0.71.2 1.8 2.7 3.3 4.4**3** 5\$A43.3 7.51.7 0.7 1.2 1.8 2.7 3.2 4.0 5 4 4.8 2.8 6.6 j. 9 0.7 j. 1 j. 8 2.6 2.9 3.1 3 5 3.1 j. 8 0.5 0.7 1.1 1.7 2.2 2.5 2.3 2 1 1.7 0.9 0.5 0.7 1.1 1.5 1.9 2.0 1.8 1.5 1.1 0.6 °C 0.5 0.8 1.0 1.3 1.5 1.5 <u>1.3 1.</u>1 0.7 0.4 © 0.6 0.7 0.9 1.1 1.1 1.1 0.9 0 7 0.4 0.3 0.6 0.7 0.9 1.0 1.0 0.9 0.8 0.6 0.3 0.2 0.6 0.7 0.9 1.0 1.1 1.1 0.9 0.8 0.4 0.3 × 0.5 0.7 1.0 1.2 1.5 1.5 1.4 1.1 0.8 0.4 0.5 0 7 1.0 1.4 1.8 2.1 1.8 1.6 1.2 0.6 0.5 0 7 1.1 1.6 2.1 2.5 2.4 2.2 1.9 1.1

1.2 2.0 2.6 2.3 1,5 0.8 0.4 0.3 0.2 0.1 0.0 0.0

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24.5 0.6 0.8 0.9 1.0 1.0 1.0 0.9 0.7 0.4 0.3

3.40,6 0.81.01.21.41.41.3100.704

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·C 0.8 0.8 1.0 a.2 1.4 1.4 1.2 1.0 0.7 0.4

C 0.8 0.7 0.8 0.9 1.0 1.0 0.8 0.6 0.4 0.2

0.5 0.7 0.8 0.9 0.9 0.8 0.6 0.5 0.3 0.2

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0.5 0.7 0.9 1.1 1.4 1.4 <u>1.3 1.1</u> 0.7 0.4 0.2

7.8 2.0 1.7 1.3 0.8 0.4 0.2 0.1 0.1 0.1 0.1 0.1 0.5 0.8 1.1 1.3 1.2 1.8 1.6 1.9 1.7 1.2 0.8 0.4 0.2 0.1 0.1 0.1 0.1 0.1 0.2 0.4 0.5 0.7 1.1 1.7 2.5 3.4 3.6 2.7 1.9 1.1 0.7 0.7 1.0 1.5 2.3 3.337 3.0 2.1 1.4 1.3 1.8 2.6 3.2 3.8 5.1 5.3 3.3 7 2 2.4 2.0 1.6 1.0 0.5 0.2 0.1 0.1 0.1 0.1 0.1 0.2 0.3 0.4 0.6 1.0 1.7 2.5 3.2 3.4 2.8 2.4 1.9 1.4 1.4 1.7 2.0 2.6 3.1 3.3 2.9 2.3 1.6 1.4 1.8 2.6 3.3 4.1 5.2 5.6 3.9 TA 3.6 3.0 1.8 1.7 0.9 0.4 0.2 0.1 0.1 0.1 0.1 0.2 0.3 0.4 0.5 0.7 1.0 1.5 2.0 1.8 1.9 2.3 2.5 2.5 2.2 2.2 2.3 2.5 2.4 2.0 1.9 1.9 1.7 1/3 1.3 1.8 2.4 2.9 2.9 2.9 1.7 2.9 2.7 1.9 1.8 1.1 0.5 0.2 0.1 0.1 0.1 0.1 0.2 0.3 0,5 0.8 1.1 1.4 1.7 1.9 1.1 1.2 1.6 2.0 2.6 3.3 3.5 2.9 2.3 1.7 1.2 1.1 1.2 1.1 1.2 1.6 2.1 2.4 2.3 2.0 1.7 0.9 2.0 2.3 1.9 1.5 0.9 0.5 0.2 0.1 0.1 0.1 0.1 0.2 0.3 0.6 1.2 1.7 2.1 2.4 2.2 0.5 0.5 0.9 1.5 2.3 3.4 3.8 2.8 1.9 1.1 0.6 0.5 0.7 0.8 0.9 1.1 1.4 1.8 2.0 1.7 1.5 1.1 0.6

> BLDG. 5 12,090 SF CLR.HGT: 22

0.4 p.7 1.0 1.3 1.7 2.0 <u>1.8 1.5</u> 1.2 0.6 p.3 0.4 0.7 1.0 1.5 2.0 2.4 2.3 2.0 1.8 1.0 0.6 C 0.8 0.7 1.0 1.6 2.3 2.8 2.9 3.1 3.3 1.9 1.1 ~ 0.9 0.7 1.1 1.6 2.4 3.1 3.6 4.7 5.4 3.3 1.8 3.3 3.1 1.9 1.8 1.1 0.5 0.2 0.1 0.1 0.1 0.1 0.1 0.1 0.3 0.7 1.3 1.9 2.1 2.6 2.5 0.3 0.4 0.6 1.1 2.0 3.2 3.8 3.0 2.0 1.1 0.6 0.5 0.6 0.7 0.8 1.1 1.6 2.5 3.2 4.0 5.4 5.8 4.1 2.2

^A3.7 3.2 1.9 1.8 1.1 0 5 0.2 0.1 0.1 0.1 0.1 0.1 0.3 0.5 0.9 1.4 1.7 2.0 2.0 0.8 0.9 1.3 1.7 2.5 3.3 3.6 3.2 2.7 1.9 1.2 1.1 1.2 1.0 0.9 1.2 1.7 2.5 3.1 3.6 4.8 5.5 3.4 1.8 7 2 2 2.7 2.0 1.9 1.2 0.6 0.3 0.1 0.1 0.1 0.1 0.2 0.3 0.4 0.6 0.8 1/1 1.6 2.0 1.6 1.7 2.1 2.3 2.5 2.4 2.4 2.6 2.9 2.7 2.0 1.9 1.9 1.4 1.0 1.2 1.7 2.4 2.9 3.0 3.2 3.4 2.0 1.1 1.9 2.2 1.9 1.5 1.0 0.5 0.3 0.1 0.1 0.1 0.1 0.1 0.3 0.4 0.5 0.7 1.0 1.5 2.1 1.8 1.8 2.1 2.4 2.4 2.1 2.1 2.5 2.9 2.6 2.1 2.0 2.1 1.7 1.3 1.3 1.6 2.1 2.5 2.4 2.1 1.9 1.1 0.6 1.5 1.8 1.8 1.4 0.8 0.5 0.3 0.1 0.1 0.1 0.1 0.1 0.2 0.4 0.5 0.7 1.1 1.7 2.5 2.8 3.0 2.7 2.4 2.0 1.7 1.6 2.1 2.6 2.9 3.3 3.2 2.6 1.9 1.3 1.2 1.4 1.8 2.1 1.8 1.6 1.2 0.7 0.4 1.9 2.3 2.0 1.7 1.1 0.6 0.3 0.1 0.1 0.1 0.1 0.1 0.2 0.4 0.6 1.0 1.5 2.1 2.9 3.2 3.6 2.8 2.1 1/3 0.9 0.8 1.2 2.0 2.8 3. 7 3.6 2.6 1.8 1.2 1.1 1.2 1.4 1.5 1.3 1.1 0.8 0.5 0.2 7.2 0.6 0.8 0.9 1.0 1.0 0.9 0.7 0.5 0.3 0.2 A3.7 3.4 1.9 1.8 1.2 0.5 0.2 0.1 0.1 0.1 0.1 0.1 0.2 0.5 1.2 1.8 1.9 2.7 2. C 1.3 0.6 0.7 0.8 0.8 0.8 0.6 0.5 0.3 0.2 0.1 3.2 3.1 2.0 1.9 1.2 0.6 0.3 0.1 0.1 0.1 0.1 0.1 0.2 0.5 1.1 1.7 1.9 3.9 3.7 A 0.9 0.6 0.7 0.8 0.9 0.8 0.7 0.6 0.4 0.2 0.2 ·C2.1 0.6 0.8 1.0 1.2 1.2 1.1 0.9 0.7 0.4 0.2 2.1 2.4 2.1 1.8 1.1/0.6 0.3 0.2 0.1 0.1 0.1 0.1 0.2 0.5 1.1 1.8 1.9 3.1 3.

BLDG. 6 14,030 SF CLR.HGT: 22' ·C2.1 0.6 0.9 1.2 1.5 1.7 1.6 1.4 1.1 0.6 0.3 0.4 0.6 0.9 1.3 1.8 2.2 2.1 1.8 1.6 0.9 0.5 0.3 0.6 0.9 1.4 2.0 2.6 2.7 2.5 2.6 1.6 1.0 0.3 0.6 0.9 134 2.2 2.9 3.2 3.9 4.9 3.0 1.6 0.3 0.6 0.9 1.4 2.2 3.1 3.7 4.9 6.0 4.3 2 3 3.2 0.5 0.9 1.4 2.2 2.9 3.1 3.7 4.5 2.8 1.5

₹ | 0.6 | 0.8 | 1.0 | 1.2 | 1.3 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.4 | 1.5 | 1.4 | 1.3 | 1.2 | 1.4 | 1.7 | 2.4 | 3.3 | 3 | 2.6 | 1.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 1.0 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0

 $\begin{bmatrix} 0,3 \\ 0,6 \\ 0,9 \\ 1,1 \\ 1,3 \\ 1,4 \\ 1,2 \\ 1,3 \\ 1,4 \\ 1,3 \\ 1,4 \\ 1,4 \\ 1,5 \\ 1,6 \\ 1,4 \\ 1,4 \\ 1,5 \\ 1,6 \\ 1,4 \\ 1,5 \\ 1,2 \\ 1,5 \\ 1,6 \\ 1,4 \\ 1,5 \\ 1,6 \\ 1$ 0.2 0.3 0.5 0.7 0.8 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.50.1 $5.0 \ 5.0$

scheme: 7

Luminaire Schedule Lum. Watts Lum. Lumens Arrangement LITHONIA KAXW LED P3 40K R4 MVOLT, +25'-0" AFG 0.900 V2_LIGHTING CORE QUBE TILT_83CRI_1000lm_6 SINGLE 0.900 LITHONIA LDN4 40 10 LO4AR LD 0.900 LSI XALM-FT-LED-HO-40, 25'-0" OVERALL POLE HEIGHT •-□ | SA SINGLE 27876 0.900

ANCHOR BASE COVER— DOUBLE NUTS ON ANCHOR BOLTS. (4) ANCHOR BOLTS PROVIDED AS PART OF FIXTURE. INSTALL BOLTS PER FIXTURE MANUFACTURER'S BOLT PATTERN. CONDUIT AS NOTED		4"x4" STEEL POLE WITH GASKETED HAND HOLE DARK BRONZE FINISH. CONNECT GROUNDING CO GROUNDING LUG INSIDE GROUT BELOW LEVELING BASE 2" CHAMFER CONCRETE BASE/RUBE EXPOSED FACES FOR SMOOTH FINISH. PAI YELLOW AS DIRECTE BY ARCHITECT OR ENGINEER ASPHALT PAVING	AND ONDUCTOR TO HANDHOLE. STUB CONDUIT 2' ABOVE TOP OF BASE NT
4-#5 VERTICAL REBAR WITH #4 HORIZONTAL REBAR TIES 12" ON CENTER. FIRST TIE SHALL BE 6" FROM BOTTOM 3500 PSI CONCRETE MINIMUM	2'-0"	#6 COPPER GROUND WIRE. DOUBLE LOOP 24" DIA. AT BOTTOM OF CONC.	

GENERAL NOTES:

THE PHOTOMETRIC CALCULATIONS WERE GENERATED IN OUR OFFICE UTILIZING PHOTOMETRIC DATA FILES FURNISHED BY THE LIGHT FIXTURE MANUFACTURES AND REASONABLE LIGHT LOSS FACTORS. THE OVERALL GRID SPACING IS 10'-0" ON CENTER. TO THE BEST OF OUR KNOWLEDGE THIS PHOTOMETRIC CALCULATION REPRESENTS THE PROPOSED HORIZONTAL MAINTAINED LIGHTING LEVELS AT GRADE, INITIAL LIGHTING LEVELS WILL BE



Calculation Summary

Overall Calculations at Grade







TYPICAL POLE BASE DETAIL

The Landing Phase 1 I Photometric Site Plan

WARE MALCOMB

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